

Engineering Summary Report

LOG-13-1.58

McColly Covered Bridge Over the Great Miami River

Logan County, Ohio

June 1997

**B U R G E S S
& N I P L E
E N G I N E E R S
A R C H I T E C T S**

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1.0 BRIDGE CONDITION

1.1 Introduction

On November 25, 1996 an inspection of the McColly Covered Bridge was performed by Ronald Mattox, Jeffrey Griffin, and Anthony Allbery of Burgess & Niple, Limited. This inspection included sounding and probing of each timber member to determine the extent of any rot or deterioration. The findings of this inspection are summarized in the following report.

Overall the McColly Covered Bridge is in "imminent" failure condition and has been closed.

1.2 Deck

Timber plank flooring is in fair condition. Dirt and moisture on the deck will create optimum conditions to promote rot.

A steel guardrail has been attached to the diagonal members of the truss. These guardrails are in generally good condition with collision damage exhibited on the right side near the rear abutment.

1.3 Superstructure

Reference Figures 1 and 2 for location of superstructure conditions identified in the following narrative.

The horizontal alignment of the bridge is good. In the vertical plane however, the bridge exhibits a sag which is most notable at the ends of the bridge. Both trusses also lean to the north.

Steel floorbeams and stringers were installed in 1959. They exhibit minor rusting and are in fair condition.

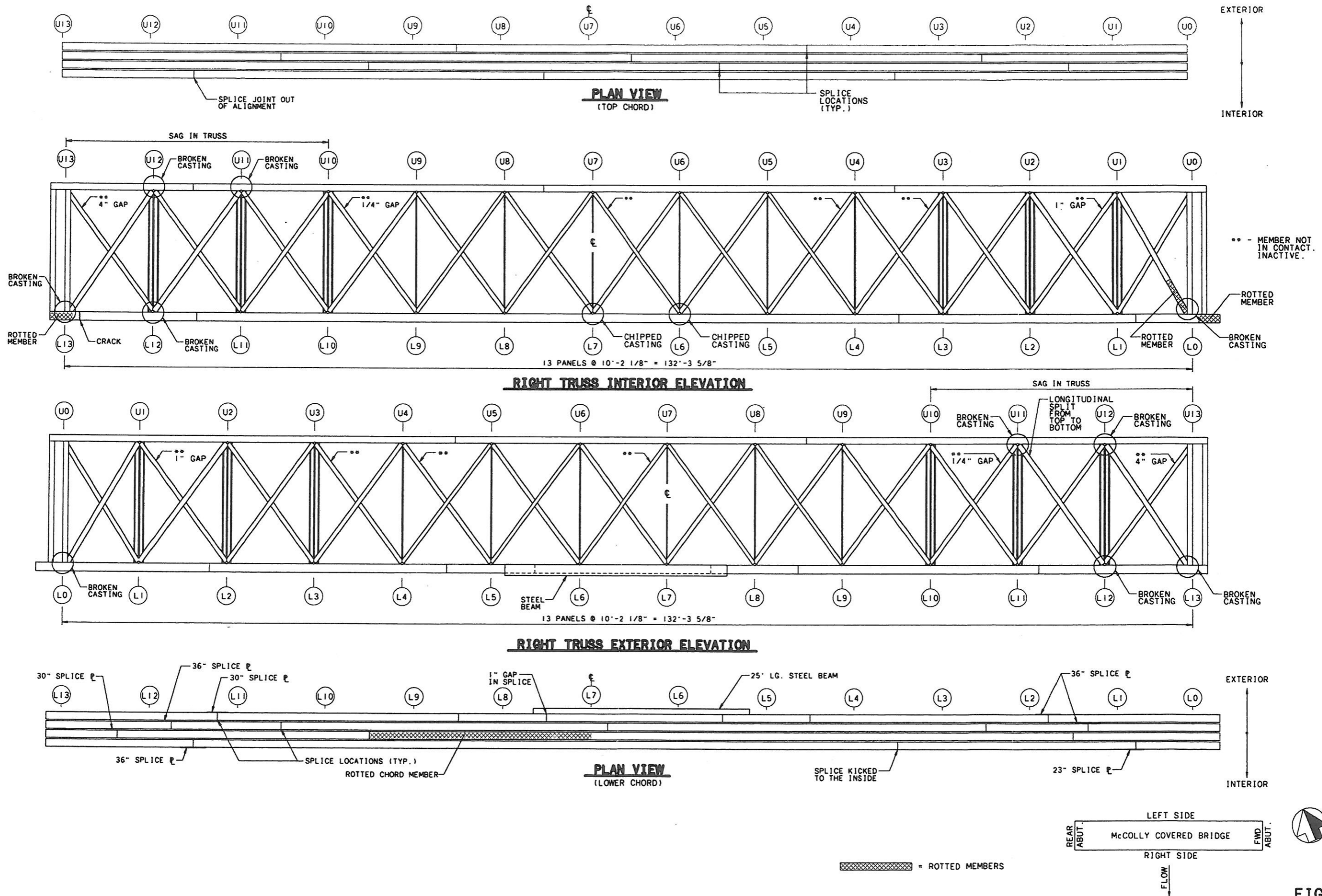


FIGURE 1

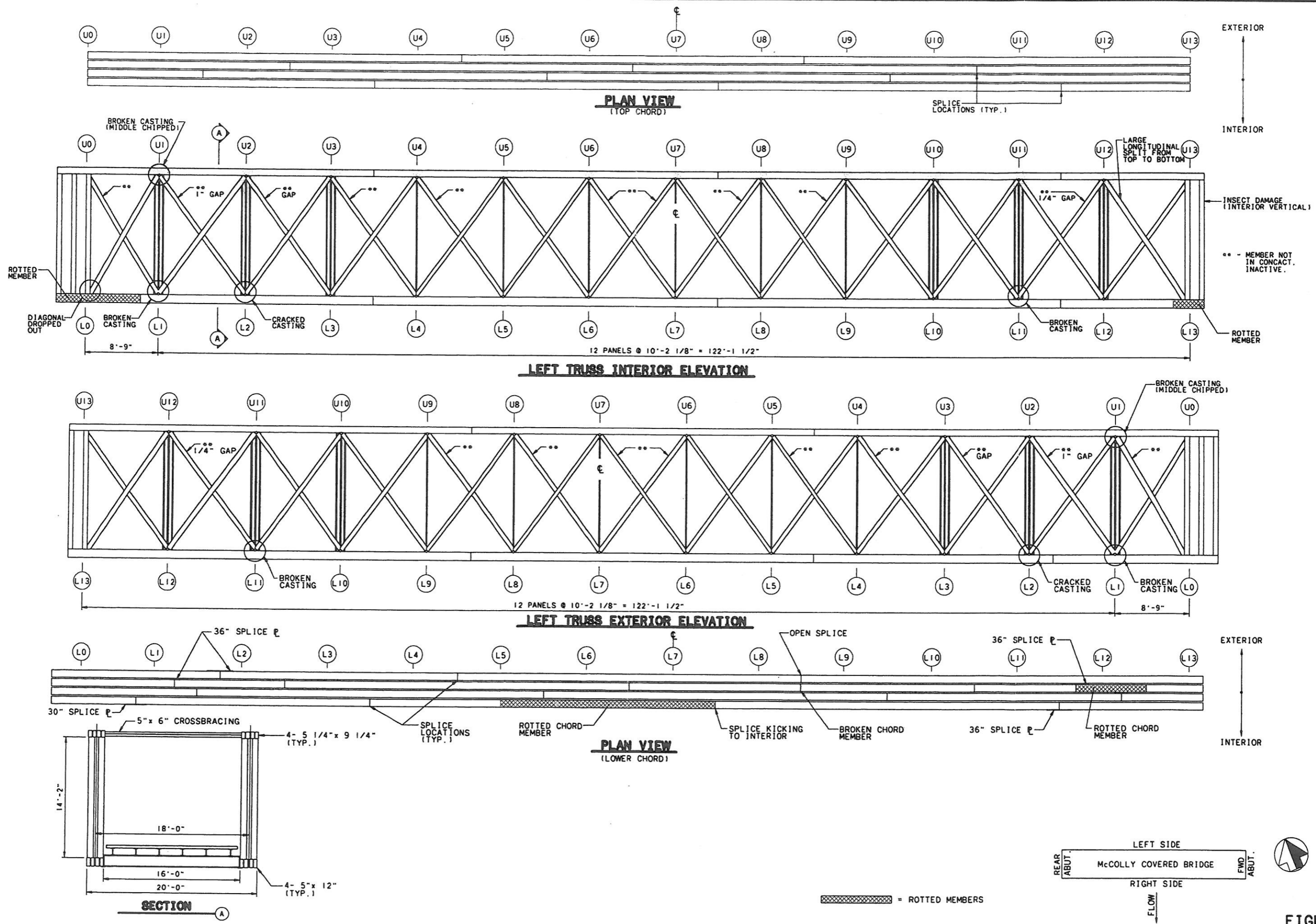


FIGURE 2

Vertical tension members at each of the intermediate panel points consist of multiple wrought iron rods which extend through both the upper and lower chords and are bolted against gib plates. In 1959, additional rods were installed at specific locations to supplement the existing rods. All rods and gib plates are in good condition. No crushing of the timber member beneath the gib plates was noted.

Timber diagonal braces and counter braces are framed squarely into cast-iron angle blocks that are framed into the upper and lower chord members. Generally the diagonals are in fair condition; however, several exhibit rot at the lower ends. Those diagonals that exhibit rot are in locations where the siding has been removed allowing water to collect on the members. Approximately 60 percent of the counter braces are loose or are completely removed from the angle block. Approximately 20 percent of the cast-iron angle blocks are cracked or completely broken.

End posts for the Howe type truss are not main load carrying members. They support the roof in the end panels and the portals. Between 1944 and 1958, the end post at the northwest corner of the bridge was moved and the diagonals were modified accordingly. The end posts are generally in good condition.

The upper chord consists of four timber members continuous for the length of the bridge. Upper chord members are in fair condition. No signs of rot, insect damage, or deterioration were found; however, a significant sag in the chord exists.

The lower chord also consists of four timber members continuous from abutment to abutment. The lower chord is in critical condition. Rot is evident at several locations along the chord. At the abutments, the rot has resulted in significant loss of section. At the individual member joints the rot has allowed the joints to open which has increased the stress in the remaining members resulting in member fractures and sagging of the superstructure. Fractures of the chord members at the abutments were noted. Steel beams have been added to the lower chords to keep them together.

Lower lateral bracing angles are in fair condition exhibiting minor surface rusting.

Upper lateral bracing consists of timber x-bracing with iron tie rods. Generally the bracing is in good condition. At one location the timber cross brace has split and has been bolted together.

In 1944 the entire roof was replaced. The roof constructed consists of new rafters on 2 foot centers, supporting wooden shingles covered with 20 gage sheet metal. The current condition of this roof is fair. At several locations, water is penetrating the roof and falling to the deck below.

The wooden plank siding is in critical condition. Approximately 30 percent of the siding is missing. The remaining planks exhibit rot and are splitting.

At each of the four corners of the bridge, the lower chord of the trusses are set on steel plates that are bolted to the abutment. The bearings are covered with dirt and debris.

1.4 Substructure

The original abutments were made of local stone. The substructures visible today are concrete. The stone abutments may have been covered with concrete. The abutments are in fair condition with minor cracking exhibited.

Both abutment seats are covered with dirt and debris. This material has collected against the lower chord and has promoted rotting of these members.

2.0 ANALYSIS

2.1 Loads

Dead loads for the primary analysis include self weight of each truss and point loads representing the roof, siding, and floor. Roof loads include the existing shingles and metal sheeting. The floor loads represent a new glued laminated floorbeam and deck system. Additional analyses were performed with a reduction of dead load. The reduction was obtained by using the existing floor system and removal of the shingles under the metal roof.

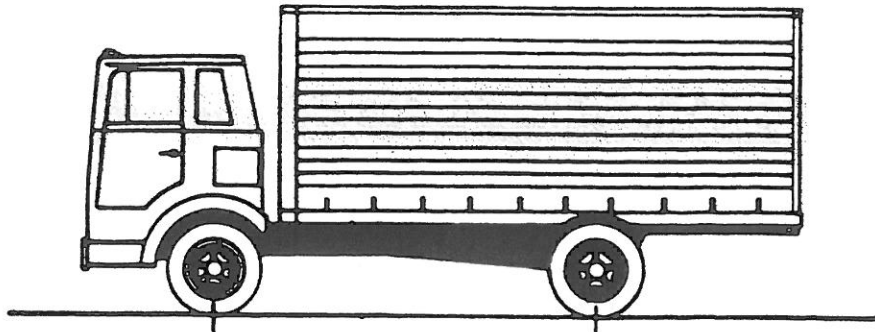
Primary live load analysis is based on American Association of State Highway and Transportation Officials (AASHTO) H15 loading. This represents a single 15 ton truck with two axles spaced at 14 feet (Figure 3). Half of the live load is applied to each truss. The live load was applied to the truss as a moving load from one end to the other to determine the maximum and minimum loads within each member.

A secondary live load representing a school bus fully loaded with children was also applied to the truss. The bus live load shown in Figure 4 was applied in the same manner as the H15 truck load.

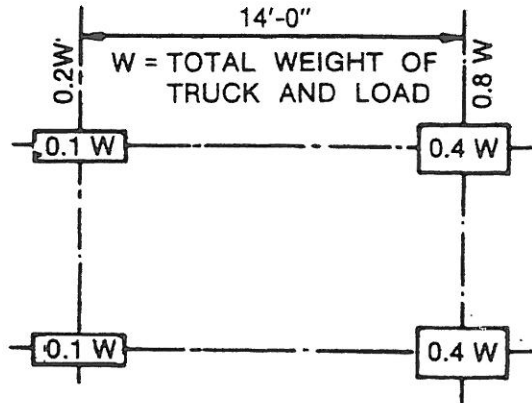
2.2 Methodology

A plane frame analysis was performed on the trusses using STAAD III release 21, developed by Research Engineers. The model created within STAAD is shown in Figure 5. Members 27 through 66 are designated as truss members, which by definition are capable of axial loads only. Members 67 through 93 are added to the truss to model the actual transfer of live loads to truss panels through the floorbeams.

Member forces from the STAAD III analysis output were transferred to a Summary Table spreadsheet (Table 2) for calculation of member stresses and load rating capacity. The summary spreadsheet also includes calculation of member properties based on field measurements, and allowable stress design values.



H 20-44	8,000 LBS.	32,000 LBS.*
H 15-44	6,000 LBS.	24,000 LBS.



CLEARANCE AND
LOAD LANE WIDTH

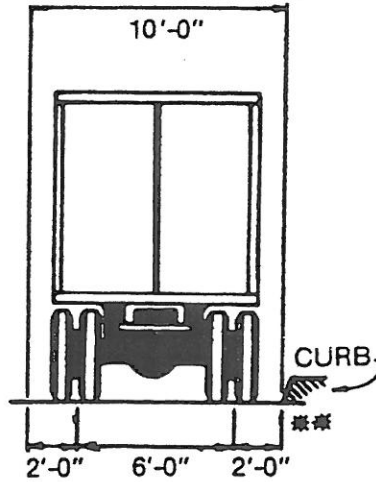


FIGURE 3

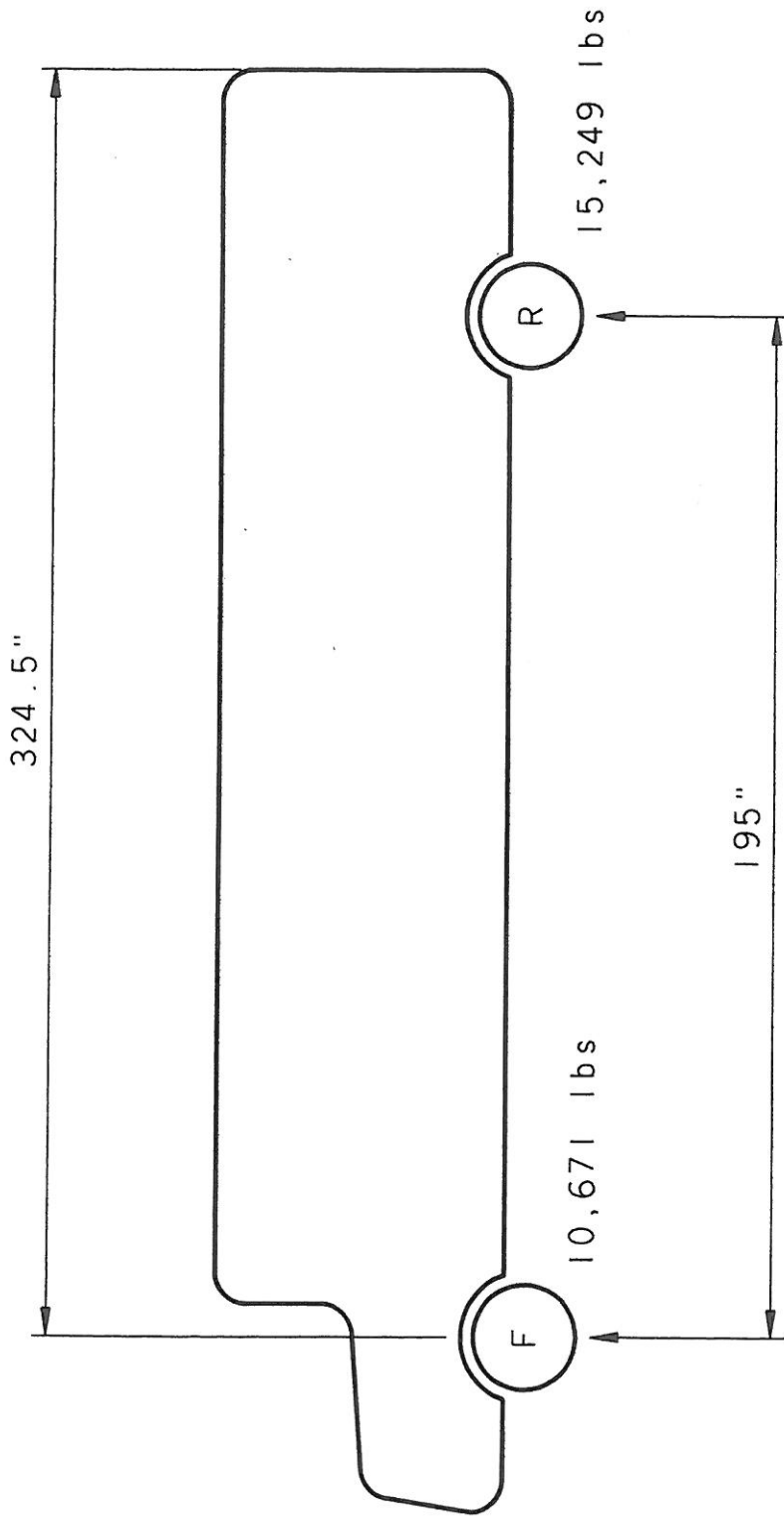


FIGURE 4

- COMPRESSION DIAGONAL
- COUNTER
- VERTICAL ROD
- JOINT #
- UPPER CHORD
- LOWER CHORD
- LIVE LOAD CARRIAGE

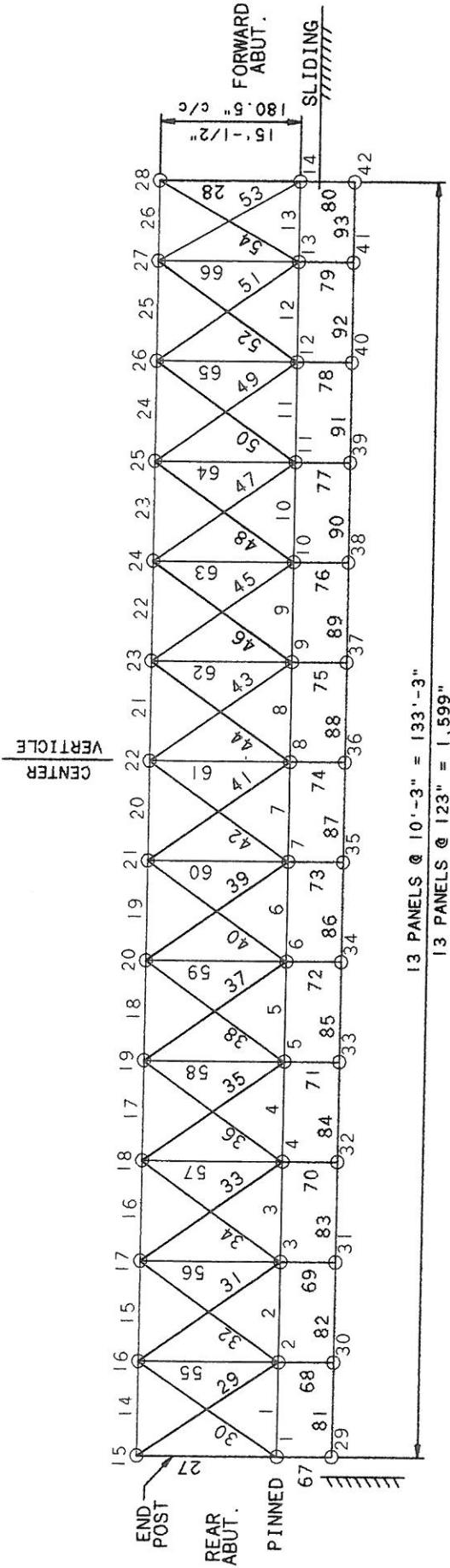


FIGURE 5

Allowable stress values are in accordance with AASHTO, 16th edition, and the *National Design Specification for Wood Construction*, 1991 edition. Timber samples from the structure were sent to the U.S. Department of Agriculture and identified as Red Pine. Tabulated values for Red Pine have been multiplied by the applicable adjustment factors to determine allowable design values (Table 1).

2.3 Member Capacity

An initial analysis was performed on the complete truss with full dead load only. This analysis indicated that all truss counters are in tension. The actual structure does not provide a tension connection for these members; therefore, they are inactive. These members were removed from the truss configuration for all subsequent analyses. Dead load compression in member 42 is less than 500 pounds. Under minimal live load, this member will be in tension. Therefore, this member has also been eliminated from subsequent analyses.

Full H15 live load was applied to the truss. This analysis indicated that under specific load conditions, the compression diagonals on both sides of the truss centerline develop tension greater than dead load compression. This indicated that a sequential analysis of the truss would be required. Several analyses have been run with an increasing percentage of live load to determine at what percent of live load compression members go into tension and become inactive. Inactive members were removed for subsequent analyses. Truss EVENTS have been established for each change in configuration up to full H15 loading.

The initial truss configuration for live load analysis is shown in Figure 6. This configuration, without counters and member 42, is valid up to 60 percent of H15 live load. This load level, defined as EVENT A, establishes the level at which members 40 and 43 are in tension and become inactive.

Figure 7 shows the truss configuration for live load analysis between EVENT A and EVENT B (0.92 H15). Beyond EVENT B, members 38 and 45 become inactive (Figure 8). This configuration is valid to EVENT C. EVENT C represents 100 percent of H15 live load.

Allowable Member Stresses (psi)
Red Pine Sawn Lumber (1.)

29-APR-97

		Adjustment Factors															Allowable					
AASHTO Reference		13.5.5.2 T 13.5.5A	13.5.5.1 T 13.5.1A		13.6.4.4	13.6.4.2 T 13.5.1A	13.6.4.3	T 13.5.1A	T 13.5.1A		13.6.4.5	13.7.3.3	T 13.5.1A		13.6.6.3							
NDS Reference		2.3.2 Append B	2.3.3 Table 4D	2.3.4 Append C	2.3.7 3.3.3	4.3.2 Table 4D	5.3.2	4.3.3, 5.3.3	4.3.4	5.3.4	2.3.8	2.3.9 3.7.1	Table 4D	4.4.3	2.3.10							
Loading	Member	Tabulated design		X	Load Duration	Wet Service	Temper- ature	Beam Stability	Size	Volume	Flat Use	Repetitive Member	Curvature	Form	Column Stability	Shear Stress	Buckling Stiffness	Bearing Area	=	Allowable		
		Value	Red Pine Table 4D																	Value	Red Pine	
					CD	CM	Ct	CL	CF	CV	Cfu	Cr	Cc	Cf	CP	CH	CT	Cb				
Dead Load	Beams & Stringers (Chords)	Fb	1,050	X	0.90	1.00	1.00	1.00	1.00										=	Fb'	945	
		Ft	625	X	0.90	1.00	1.00	1.00	1.00										=	Ft'	563	
		Fv	65	X	0.90	1.00	1.00	1.00								1.00			=	Fv'	59	
		Fc	440	X		0.67	1.00											1.00		=	Fc '	295
		Fc	725	X	0.90	0.91	1.00		1.00							1.00				=	Fc'	594
		E	1,100,000	X		1.00	1.00													=	E'	1,100,000
		Fg	880	X	0.90	1.00	1.00													=	Fg'	792
	Posts & Timbers (Vert.) (Diag.)	Fb	1,000	X	0.90	1.00	1.00	1.00	1.00											=	Fb'	900
		Ft	675	X	0.90	1.00	1.00	1.00	1.00											=	Ft'	608
		Fv	65	X	0.90	1.00	1.00	1.00								1.00				=	Fv'	59
		Fc	440	X		0.67	1.00											1.00		=	Fc '	295
		Fc	775	X	0.90	0.91	1.00		1.00							1.00				=	Fc'	635
		E	1,100,000	X		1.00	1.00													=	E'	1,100,000
		Fg	880	X	0.90	1.00	1.00													=	Fg'	792
Foot Notes									2	3	4	4	3	5	6		4					
Live Load	Beams & Stringers (Chords)	Fb	1,050	X	1.20	1.00	1.00	1.00	1.00										=	Fb'	1,260	
		Ft	625	X	1.20	1.00	1.00	1.00	1.00										=	Ft'	750	
		Fv	65	X	1.20	1.00	1.00	1.00								1.00			=	Fv'	78	
		Fc	440	X		0.67	1.00											1.00		=	Fc '	295
		Fc	725	X	1.20	0.91	1.00		1.00							1.00				=	Fc'	792
		E	1,100,000	X		1.00	1.00													=	E'	1,100,000
		Fg	880	X	1.20	1.00	1.00													=	Fg'	1,056
	Posts & Timbers (Vert.) (Diag.)	Fb	1,000	X	1.20	1.00	1.00	1.00	1.00											=	Fb'	1,200
		Ft	675	X	1.20	1.00	1.00	1.00	1.00											=	Ft'	810
		Fv	65	X	1.20	1.00	1.00	1.00								1.00				=	Fv'	78
		Fc	440	X		0.67	1.00											1.00		=	Fc '	295
		Fc	775	X	1.20	0.91	1.00		1.00							1.00				=	Fc'	846
		E	1,100,000	X		1.00	1.00													=	E'	1,100,000
		Fg	880	X	1.20	1.00	1.00													=	Fg'	1,056
Foot Notes			9		7				2	3	4	4	3	5	8		4					

1. Red Pine for truss members is Select Structural
2. (For d > 12") CF = (12/d)**1/9 = 1.0 (not applicable to McColly)
3. Applies to glued laminated members, not sawn lumber
4. Not applicable to timbers
5. For circular or diamond sections
6. Factors for CP (dead load) =

McColly U.C.	0.89
McColly Diag.	0.90
7. AASHTO = 1.15 increased for truss configuration to 1.2
8. Factors for CP (live load) =

McColly U.C.	0.85
McColly Diag.	0.86
9. Base design values for wet service conditions, actual conditions will be better
10. Allowable stress for wrought iron = 20,000 psi (per AASHTO)

Table 1

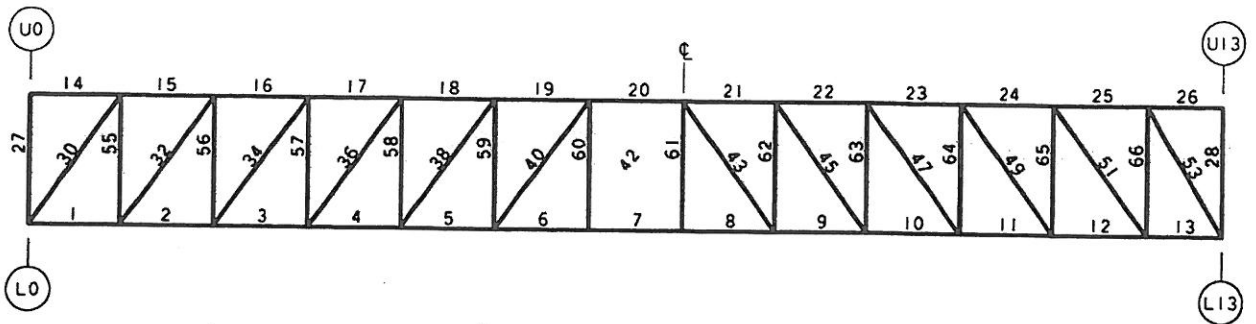


FIGURE 6: 0.0H15 → 0.60H15
EVENT A

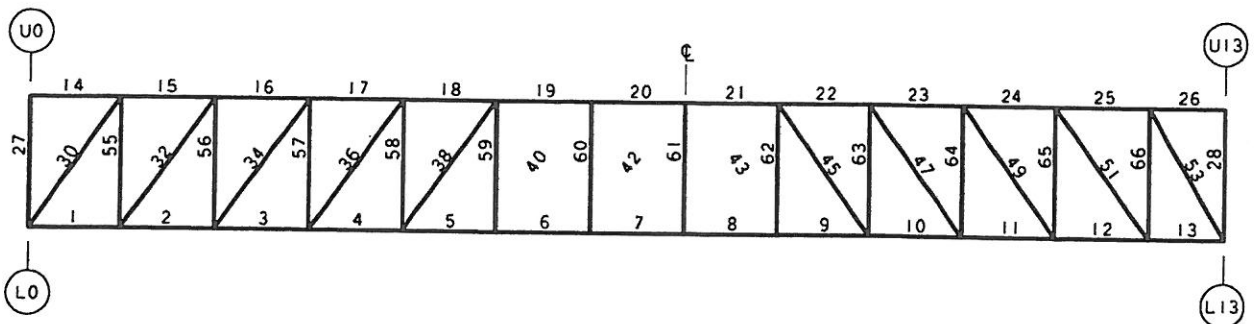


FIGURE 7: .060H15 → 0.92H15
EVENT A → EVENT B

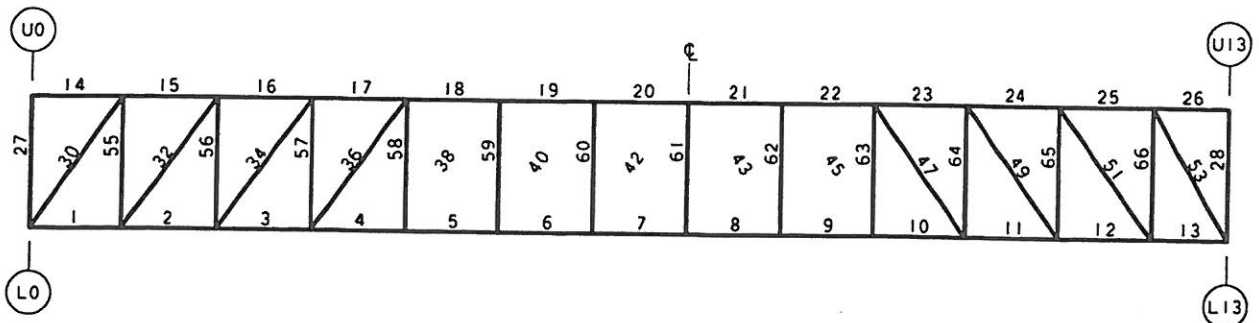


FIGURE 8: 0.92H15 → 1.00H15
EVENT B → EVENT C

Table 2 is a summary of the loads, stresses, and load rating for each member for sequential live loading to full H15. End posts, compression diagonals, counters, and verticals (members 27 through 66) are designated as truss members. The shaded areas in Table 2, for bending end shear, do not apply for these members.

As shown in the Rating columns, members 4, 5, 9, and 10 are rated for less than 10 tons.

A similar analysis was performed using the school bus live load. Results provided in Table 3 indicate that all members are capable of withstanding this live load.

Interaction Analysis - Capacities and ratings for members shown in Tables 2 and 3 are based on axial, shear, and bending forces acting separately on each individual member. The lower and upper chords are actually acted upon by a combination of axial and bending forces simultaneously. For these members, a restriction based on the interaction of axial and bending stresses is also imposed. The Comment column in Tables 2 and 3 indicates members exceeding the interaction requirement. Additional analyses were performed to determine the maximum allowable load due to this restriction. A maximum load of $0.55 \times H15$ (8.25 tons) was established. Table 4 provides the member ratings and interaction values at this load level.

Results of the interaction analysis also indicate that the bridge cannot carry the fully loaded school bus.

In summary, the interaction analysis indicates that the rehabilitated bridge would have to be posted for 8 tons and could not be used by fully loaded school buses.

2.4 Member Capacity with Piers

At the request of the Logan County Engineer's office, an additional interaction analysis was performed to determine the allowable load capacity of the rehabilitated bridge if piers were added. Our STAAD III input was subsequently revised to assume truss supports at Joints 3 and 12.

Results of the interaction analysis for this condition indicate the rehabilitated bridge can support a full H15 loading. Table 5 provides the member ratings and interaction values at this load level if two pier supports are added. It should be noted that tension rods for Members 56 and 65 experience compression when pier supports are added at Joints 3 and 12. These members would require replacement if piers are added.

3.0 RECOMMENDATIONS

To support an H15 loading, the following repairs are necessary:

- Clean and paint existing floor system.
- Replace timber decking.
- Replace broken or deteriorated siding boards. Boards in good condition would be reused.
- Replace deteriorated, rotted, or insect infested members located in Figures 1 and 2.
- Supplement vertical rods 56 and 65 with compression members.
- Install tension rods on each side of lower chords.
- Restore original configuration of end post and first panel of left truss.
- Provide tension connection for end posts.
- Add pier supports.
- Repaint structure.
- Cover members with fire retardant.
- Replace bearings.
- Remove shingles and replace metal roof with new metal roof.

Based on the best cost data we have at this time, we estimate the construction cost to perform these repairs would range from \$210,000 to \$245,000.

Burgess & Niple recommends the above repairs be performed if the rehabilitated bridge is to carry the H15 loading (Figure 3) or the lesser weighing school bus loading (Figure 4). Without the addition of piers, the maximum load which could be supported by the rehabilitated bridge is only 8 tons.