

## **Load Rating Report**

### **Bickham Covered Bridge over the South Fork of the Great Miami River**

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**Logan County, Ohio**

**October 2001**



**BURGESS & NIPLE**

## Introduction

On July 10, 2001, Burgess & Niple Ltd. (B&N) was contracted by the Logan County Engineer's office to conduct a load rating analysis of the proposed rehabilitated truss and floor systems on the Bickham Covered Bridge over the South Fork of the Great Miami River. This timber Howe truss bridge can be found along County Road 38 in Richland Township near Indian Lake. The Smith Bridge Company of Toledo, Ohio built this 98-foot long structure in 1877. In 1959, the wooden floor joist system was replaced with steel floor beams and stringers, and the truss was strengthened. The Logan County Engineer's office is in the process of developing rehabilitation plans for this structure. The purpose of this analysis is to provide a recommendation for live load restrictions on this covered bridge following the proposed rehabilitation.

As defined in a scope of services, B&N's responsibilities included the following:

- 1.) Field Survey – A site visit was conducted to obtain general photographs of the site, to estimate steel section loss in the floor beams and stringers, and to obtain a timber sample in order to determine the species.
- 2.) Species Identification – The sample obtained during the Field Survey was mailed to a timber specialist for identification. This identification was necessary in an effort to estimate the allowable strength of the existing members. It is our understanding that the rehabilitation will utilize replacement timbers of the same species and grade.
- 3.) Load Rating Analysis – A load rating analysis was conducted utilizing the Ohio Legal Loads (2F1, 3F1, 4F1, and 5C1), a standard school bus loading, and an H15 loading applied to the rehabilitated truss and floor systems. All truss and floor member dimensions as proposed in the rehabilitation plans were provided to B&N by the Logan County Engineer's office.
- 4.) Report – This document summarizes the results of the analysis.

## Methodology

The floor system was analyzed by hand calculations assuming simply supported floorbeam supports and continuous stringer supports. The stringers span continuously over one floorbeam. The start and end of adjacent stringers are staggered longitudinally such that no two adjacent stringers terminate at the same floorbeam. The existing wood decking is to be replaced during the rehabilitation with either nominal 3"x 4" or nominal 3"x 6" nail laminated Dense Commercial Southern Pine species decking boards. These decking boards will span transversely across the existing steel stringers. The existing stringers and floorbeams will be reused during the rehabilitation. During the "Field Survey" portion of our work, section loss on the floorbeams and stringers was estimated. After measurements were taken, the stringers showed no appreciable section loss. However, the floorbeams had enough section loss to justify a reduction in section properties. Therefore, a revised floorbeam cross section was approximated for use in the floor system load rating.

In order to determine the allowable design values for the truss members, two timber samples were obtained from the forward end and inside face of the right lower chord member on August 6, 2001. These samples were sent to the U.S. Department of Agriculture for testing. Both samples were identified as White Pine. Tabulated values for Select Structural White Pine timber have been multiplied by the applicable adjustment factors to determine the allowable design values (Table 1).

A plane frame analysis was performed on the trusses using the STAAD III design software (Release 22.3W), developed by Research Engineers. The model created within STAAD III is shown in Figure 1. Members 1 through 16 were designated as chord members, which are capable of transferring axial and shear loads as well as moments. Members 17 through 41 were designated as truss members, which are capable of transferring axial loads only. It was our understanding that the rehabilitated structure will maintain existing member continuities (i.e. existing connections will not be altered). Consequently, all diagonal members (Members 19 through 34) were modeled as incapable of transferring tensile forces.

Influence lines were used to determine the maximum live load effect on each truss member. Influence lines were generated for each truss member by determining each member's response to a unit load placed individually at each floorbeam location. The responses were determined utilizing a STAAD III model. Any diagonals that went into tension were removed to allow a redistribution of loads. Additional STAAD III runs were executed to determine floorbeam reactions due to each live load truck moving across the length of the structure. These floorbeam reactions for each position of the given live load truck were then superimposed on each member's influence line to determine the maximum live load effect on each member.

Member forces and moments from the STAAD III analysis output were transferred into summary table spreadsheets (See Tables 2-7) for calculation of member stresses and load rating capacity. The summary table spreadsheets also include calculations of member properties based on field measurements, and allowable stress design values.

The allowable stress values used in this report are in accordance with the *16<sup>th</sup> edition of the AASHTO Specifications for Highway Bridges* including the *1999 interim*, and the *1997 Allowable Stress Design (ASD) National Design Specification (NDS) for Wood Construction, with 1999 interim*.

### Loading Types

The dead loads for the truss analysis included self-weight of each truss member and point-loads representing the roof, siding, and floor systems. The roof loads included the existing shingles, metal sheeting, and all roof-supporting members. The floor loads assumed either nominal 3"x 4" or nominal 3"x 6" nail laminated decking boards supported on steel stringers and floorbeams.

The dead loads for the floor system analysis only included self-weight. It is our understanding that the rehabilitated structure will not have an asphalt overlay applied.

The truss and floor system live load analyses were based on each of the Ohio Legal Loads (2F1, 3F1, 4F1, and 5C1), a standard school bus loading, and an H15 truck loading (see Figure 2). It was determined that only 67% of a given truck could be transferred into any one given truss plane. The live loads were moved across the structure in two-foot increments with resulting loads applied to the truss through the floorbeams.

### **Member Capacities**

The allowable capacities for the timber members were based on the *1997 ASD NDS for Wood Construction, with 1999 interim*. The allowable capacity of truss and decking members were based on the *NDS* allowable design values for Select Structural White Pine and Dense Commercial Southern Pine respectively multiplied by the appropriate adjustment factors (Floor System Deck Load Rating and Table 1).

The truss chord members are capable of carrying combined axial and bending stresses. Consequently, their capacities are governed by the additional requirements of an interaction equation described in article 3.9 of the *NDS* manual.

The allowable capacities for the steel members that were added during the 1958 bridge strengthening rehabilitation are based on the typical steel yield strength for that time period (33ksi).

### **Member Stresses**

Member stresses were broken down between stresses due to dead loads and stresses due to live loads. Bending and compression (perpendicular to the grain) stresses were computed for the nail laminated decking members. Bending and shear stresses were computed for the stringers and floorbeams. Axial, shear, and bending stresses were calculated for each member of the truss system. These stresses were used to determine each member's load rating as well as the interaction equation for the upper and lower chords. For the interaction equation, where axial and bending stresses were combined, the live load stresses for each position of the truck across the length of the structure were determined and combined individually to determine the most critical load case.

### **Member Load Ratings**

While both operating and inventory ratings were provided for all steel members, operating ratings were only provided for wood members. This was a result of the *NDS* only providing for allowable stress design. Consequently, there is no beta factor to generate a distinction between inventory and operating values for wood members . Therefore, if the timber rating values in this report fall below 100% of the gross vehicle weight (a factor of less than 1.0), the bridge should be posted.

### **Floor System Summary (refer to Appendix for addition information)**

Both 3x4 and 3x6 decking members were load rated. It was determined that 3x4 members were under rated for H15 and 2F1 trucks (0.83 and 0.99 respectively). Consequently, it is our recommendation that 3x6 members be used in the rehabilitation design. Dead loads for all other members were based on 3x6 decking members.

While the stringer bending stress inventory rating for the H15, 2F1, 3F1, 4F1, and 5C1 trucks fall below 100% (0.70, 0.84, 0.75, 0.81, and 0.75 respectively), the stringer operating ratings for these trucks are sufficient (above 100%) and do not require bridge posting for any of the studied loads.

Similarly, while the floorbeam bending stress inventory rating for the H15, 2F1, 3F1, 4F1, and 5C1 trucks fall below 100% (0.88, 0.89, 0.63, 0.56, and 0.65 respectively), the floorbeam operating ratings for all of the trucks except the 4F1 are sufficient (above 100%) and do not require bridge posting. The operating rating for the floorbeams for a 4F1 truck would require a 25 gross ton posting. (Note: this rating is for the floorbeams ONLY. The trusses that support the floorbeams have lower ratings.).

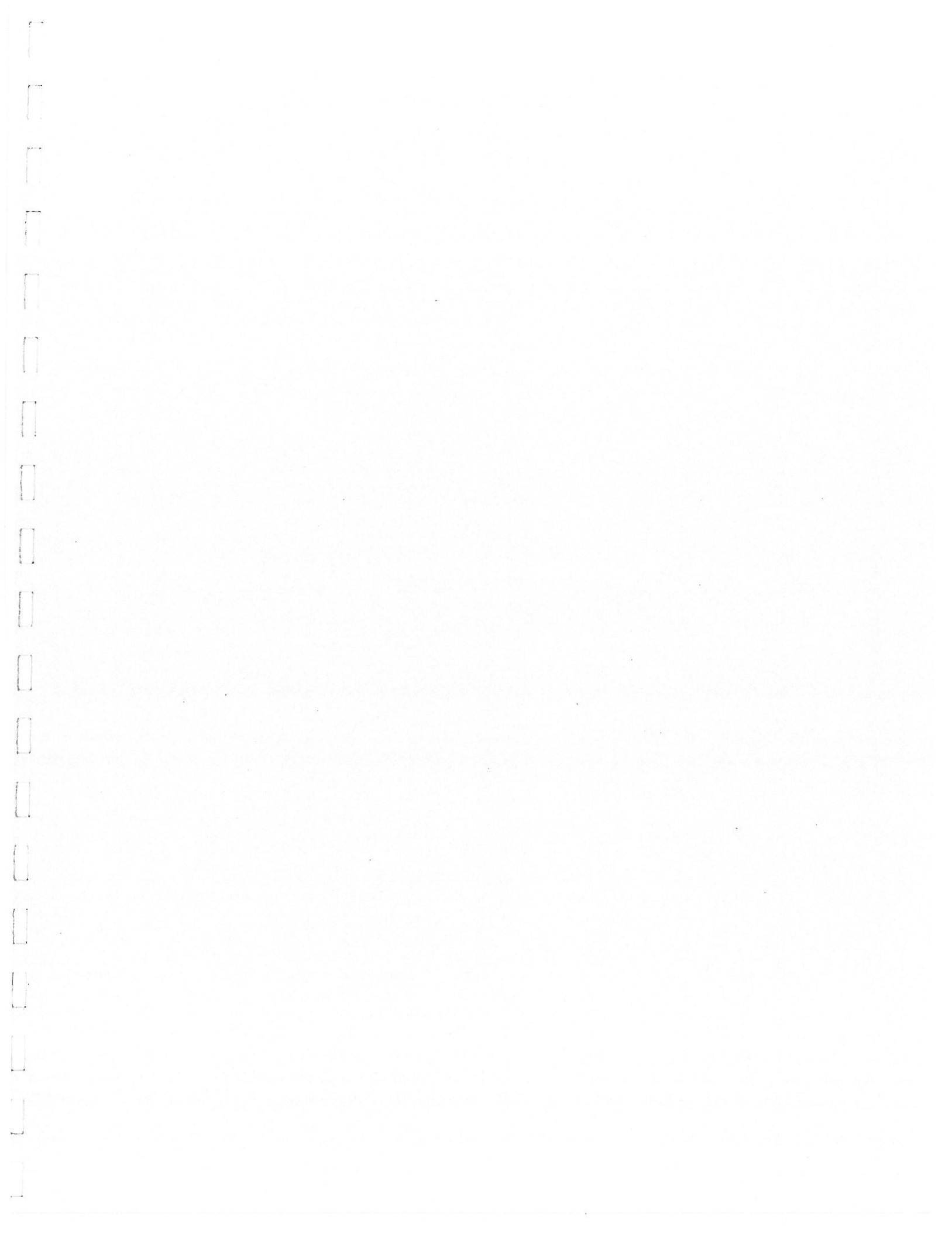
### **Truss System Summary (refer to Appendix for Tables 2 through 7)**

While truck axle spacing and axle load distribution provided a great deal of variation in load rating results, members 27 and 34 (end compression diagonals) proved to control the truss load rating (AND overall bridge rating) for each of the trucks studied. If these members are not further strengthened during a subsequent rehabilitation, the following load restrictions on the structure should be implemented:

<u>Loading Type</u>	<u>Rating Factor</u>	<u>Gross Vehicle Weight Allowed</u>
H15	0.65	9.7 tons
School Bus	0.79	10.3 tons
2F1	0.60	9.0 tons
3F1	0.43	9.9 tons
4F1	0.37	10.0 tons
5C1	0.33	13.2 tons

Furthermore, based on load rating goals of the proposed rehabilitation, Tables 2 through 7 can be used to determine what additional member modifications are required.

It should be noted that the interaction equations exceed the allowable value (greater than 1.0) for the 3F1, 4F1, and 5C1 trucks. However, the amount of overstress in the end two bays of compression diagonals exceeds the amount of overstress due to the interaction equation applied to the upper chord.



JOB NO. 30099JOB NAME Bickham Covered BridgeSUBJECT SECTION PROPERTIES PREPARED BY MAK DATE 8/8/01 CHECKED BY TMB DATE 9/3/01MEMBER: W16x40 FloorbeamsSECTION OR LOCATION: TypicalSection Depth = 16.01Section Width = 6.993

100% Section

Areas of Loss

Data for X-X Axis

Data for Y-Y Axis

Shaded cells are fields requiring input by preparer.

Description b (in.) h (in.) A (in<sup>2</sup>) y (in.) D=d-y (in) Ay (in<sup>2</sup>) AD<sup>2</sup> (in<sup>4</sup>) I<sub>object</sub> (in<sup>4</sup>) x (in.) D=d-x (in) Ax (in<sup>2</sup>) AD<sup>2</sup> (in<sup>4</sup>) I<sub>object</sub> (in<sup>4</sup>)

A1	6.9950	0.5050	3.532	0.233	7.749	0.892	212.140	0.075	0.000				
A2	0.3050	15.0000	4.575	8.005	-0.003	36.623	0.000	85.781	0.000				
A3	6.9950	0.5050	3.532	15.748	-7.746	55.628	211.925	0.075	0.000				
A4													
A5													
A6													
Totals			11.63995			93.14	424.06	85.93		0.00	0.00		
Rectangle 1	3.0000	0.0625	0.188	0.474	7.528	0.089	10.626	0.000	-2.000	2.000	-0.375	0.750	0.141
Rectangle 2	3.0000	0.0625	0.188	0.474	7.528	0.089	10.626	0.000	2.000	-2.000	0.375	0.750	0.141
Rectangle 3	3.0000	0.0625	0.188	15.526	-7.524	2.911	10.615	0.000	-2.000	2.000	-0.375	0.750	0.141
Rectangle 4	3.0000	0.0625	0.188	15.526	-7.524	2.911	10.615	0.000	2.000	-2.000	0.375	0.750	0.141
Rectangle 5													
Rectangle 6													
Rectangle 7													
Rectangle 8													
Rectangle 9													
Rectangle 10													
Triangle 1													
Triangle 2													
Triangle 3													
Triangle 4													
Triangle 5													
Totals			0.750			6.00	42.48	0.00		0.00	3.00	0.56	

Axis:	X-X	Y-Y											
d = Ay/A =	8.00	0.00											
d' = Depth - d =	8.01	6.995 in											
I = $\Sigma AD^2 + I_{object}$ =	510.00	0.00 in <sup>4</sup>											
r = (IA) <sup>1/2</sup> =	6.62	0.00 in											
S = I/d =	63.73	#DIV/0!	in <sup>3</sup>										
S' = I/d' =	63.69	0.00 in <sup>3</sup>											
A =	11.64	in <sup>2</sup>											
Area		lb/ft											
Selfweight (steel) = A(490 pcf)/(144 si/sf) =	39.61												
Percent Loss =													

Section With Loss	X-X	Y-Y											
Axis:													
d = Ay/A =	8.00	0.00											
d' = Depth - d =	8.01	7.00 in											
I = $\Sigma AD^2 + I_{object}$ =	467.51	-3.56 in <sup>4</sup>											
r = (IA) <sup>1/2</sup> =	6.55	#NUM!	in										
S = I/d =	58.42	#DIV/0!	in <sup>3</sup>										
S' = I/d' =	58.38	-0.51 in <sup>3</sup>											
A =	10.89	in <sup>2</sup>											
Percent Loss =	6.4%												

## Bickham Covered Bridge Floor System Load Rating

Actual Board Width (in.): 2.5  
Span Length 'L' (ft.): 22.21

Note: Self weight of decking members was determined to be negligible

Decking	Heavy Axle Load (kips)	Wheel Load (k)	Tire Contact Area (in. <sup>2</sup> )	Parallel to Traffic (in.)	Transverse to Traffic (in.)	Number of Boards Tire Rests on	Effective Wheel Load P' per Board (k)	M <sub>max</sub> due to L.L.	Live Load Bending Stress, fb (psi) (using...)	Live Load Compression Stress, fc (psi) (using...)
H15-44	24	12	120	15.00	17.32	6.00	2.00	0.88	3x4's	3x6's
School Bus	15.25	7.625	76.25	15.00	13.81	6.00	1.27	0.56	1318	534
Ohio 2F1	20	10	100	15.00	15.81	6.00	1.67	0.74	1729	700
Ohio 3F1	17	8.5	85	15.00	14.58	6.00	1.42	0.65	1470	595
Ohio 4F1	14	7	70	15.00	13.23	6.00	1.17	0.51	1210	490
Ohio 5C1	17	8.5	85	15.00	14.58	6.00	1.42	0.63	1470	595
				AASHTO 3.25	AASHTO 3.25				87	87
				AASHTO 3.30	AASHTO 3.30					

## Allowables Assuming Dense Commercial Southern Pine Nail Laminated Decking

	Design Value (psi)	Cd	Cm	Ct	Cl	Cf	Multipliers			
	Value (psi)	1.00	1.00	1.00	1.00	1.04	CV	Cu	Ct	Cf
Fb	1650	1.00	1.00	1.00	1.00	1.04	1.00	1.00	1.00	1.00
Fcl	660	1.00	1.00	1.00	1.00	1.04	1.00	1.00	1.00	1.00

## Rating Factors

Loading Type	Bending Stress Rating Factor	Compression Stress Perpendicular to the grain Rating Factor
H15-44	= (Allowable Stress-DL)/(Live Load Stress) Using 3x4's	= (Allowable Stress-DL (negligible))/(Live Load Stress) Using 3x6's
School Bus	0.83	0.83
Ohio 2F1	1.30	2.04
Ohio 3F1	0.99	3.21
Ohio 4F1	1.17	2.45
Ohio 5C1	1.42	2.88

## Allowable Gross Vehicle Load (Tons)

Loading Type	Vehicle Gross Load (tons)	Bending Stress		Compression Stress Perpendicular to the grain	
		Allowable Gross Load (tons) Using 3x4's	Allowable Gross Weight Using 3x6's	Allowable Gross Load (tons) Using 3x4's	Allowable Gross Load (tons) Using 3x6's
H15-44	15	12.41	30.64	80.38	80.38
School Bus	13	16.92	41.79	109.63	109.63
Ohio 2F1	15	14.89	36.76	96.45	96.45
Ohio 3F1	23	26.86	66.32	173.99	173.99
Ohio 4F1	27	38.28	94.54	248.02	248.02
Ohio 5C1	40	46.71	115.34	302.59	302.59

**Bickham Covered Bridge**  
**Floor System Load Rating**

**Stringers**

Stringer Area, A ( $\text{in}^2$ ): 7.08  
 Stringer Modulus, S ( $\text{in}^3$ ): 20.90  
 Web Area ( $\text{in}^2$ ): 1.94  
 Fy (ksi): 33.00

<<----(Steel added in 1957 when allowables were less than 36ksi)

Loading Type	Bending				Shear		
	Mmax due to D.L. (k*ft.)	Mmax due to L.L.+I (k*ft.)	D.L. Bending Stress (psi)	Max. L.L. + I Bending Stress (psi)	D.L. Shear Stress (psi)	Max. L.L. + I Shear force (kip)	Max. L.L. + I Shear Stress (psi)
H15-44	0.53	37.20	304.31	21358.85	211.60	15.20	7835.05
School Bus	0.53	23.60	304.31	13550.24	211.60	9.70	5000.00
Ohio 2F1	0.53	31.00	304.31	17799.04	211.60	13.40	6907.22
Ohio 3F1	0.53	35.00	304.31	20095.69	211.60	18.90	9742.27
Ohio 4F1	0.53	32.40	304.31	18602.87	211.60	18.60	9587.63
Ohio 5C1	0.53	35.00	304.31	20095.69	211.60	18.60	9587.63

**Rating Factors**

Loading Type	Bending Stress	
	Inventory Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress*1.67)	Operating Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress)
H15-44	0.70	1.17
School Bus	1.11	1.85
Ohio 2F1	0.84	1.41
Ohio 3F1	0.75	1.25
Ohio 4F1	0.81	1.35
Ohio 5C1	0.75	1.25

Loading Type	Shear Stress	
	Inventory Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress*1.67)	Operating Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress)
H15-44	1.92	3.21
School Bus	3.01	5.03
Ohio 2F1	2.18	3.64
Ohio 3F1	1.55	2.58
Ohio 4F1	1.57	2.63
Ohio 5C1	1.57	2.63

**Allowable Gross Vehicle Load (Tons)**

Loading Type	Vehicle Gross Load (tons)	Bending Stress	
		Inventory Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight	Operating Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight
H15-44	15	10.55	17.61
School Bus	13	14.41	24.06
Ohio 2F1	15	12.66	21.14
Ohio 3F1	23	17.19	28.71
Ohio 4F1	27	21.80	36.40
Ohio 5C1	40	29.89	49.92

Loading Type	Vehicle Gross Load (tons)	Shear Stress	
		Inventory Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight	Operating Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight
H15-44	15	28.86	48.19
School Bus	13	39.19	65.45
Ohio 2F1	15	32.73	54.67
Ohio 3F1	23	35.59	59.43
Ohio 4F1	27	42.45	70.89
Ohio 5C1	40	62.89	105.02

**Bickham Covered Bridge**  
**Floor System Load Rating**

**Floorbeams**

**Stringer Reactions**

Loading Type	Control	Max. LL+I Stringer Reactions (k.)	Stringer Reaction (k.)					
			R1	R2	R3	R4	R5	R6
H15-44	Bending	15.60	0.00	9.20	6.40	6.40	9.20	0.00
	Shear		15.60	0.00	12.79	2.81	0.00	0.00
School Bus	Bending	9.90	0.00	5.84	4.06	4.06	5.84	0.00
	Shear		9.90	0.00	8.12	1.78	0.00	0.00
Ohio 2F1	Bending	15.40	0.00	9.09	6.31	6.31	9.09	0.00
	Shear		15.40	0.00	12.63	2.77	0.00	0.00
Ohio 3F1	Bending	21.90	0.00	12.92	8.98	8.98	12.92	0.00
	Shear		21.90	0.00	17.96	3.94	0.00	0.00
Ohio 4F1	Bending	24.40	0.00	14.40	10.00	10.00	14.40	0.00
	Shear		24.40	0.00	20.01	4.39	0.00	0.00
Ohio 5C1	Bending	21.20	0.00	12.51	8.69	8.69	12.51	0.00
	Shear		21.20	0.00	17.38	3.82	0.00	0.00

Floorbeam Area, A ( $\text{in}^2$ ): 10.89  
Floorbeam Modulus, S ( $\text{in}^3$ ): 58.38

Fy (ksi): 33.00

<<----(Steel added in 1957 when allowables were less than 36ksi)

Loading Type	Bending				Shear			
	Mmax due to D.L. (k*ft.)	Mmax due to L.L. (k*ft.)	D.L. Bending Stress (psi)	Max. L.L. Bending Stress (psi)	D.L. Shear Force (kips)	Max. L.L. Shear Force (kips)	D.L. Shear Stress (psi)	Max. L.L. Shear Stress (psi)
H15-44	8.84	78.05	1817.06	16043.17	2.27	23.16	312.67	3190.08
School Bus	8.84	49.53	1817.06	10180.88	2.27	14.70	312.67	2024.79
Ohio 2F1	8.84	77.03	1817.06	15833.50	2.27	22.86	312.67	3146.76
Ohio 3F1	8.84	109.56	1817.06	22520.04	2.27	32.52	312.67	4479.34
Ohio 4F1	8.84	122.05	1817.06	25087.36	2.27	36.23	312.67	4990.36
Ohio 5C1	8.84	106.05	1817.06	21798.56	2.27	31.47	312.67	4334.71

**Rating Factors**

Loading Type	Bending Stress		Operating Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress*1.67)
	Inventory Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress*1.67)	Operating Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress)	
H15-44	0.88		1.47
School Bus	1.39		2.31
Ohio 2F1	0.89		1.49
Ohio 3F1	0.63		1.05
Ohio 4F1	0.56		0.94
Ohio 5C1	0.65		1.08

Loading Type	Shear Stress		Operating Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress)
	Inventory Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress*1.67)	Operating Rating Factor =(Allowable Stress/1.3-D.L. Stress)/(Live Load Stress)	
H15-44	4.71		7.86
School Bus	7.41		12.38
Ohio 2F1	4.77		7.96
Ohio 3F1	3.35		5.60
Ohio 4F1	3.01		5.02
Ohio 5C1	3.46		5.78

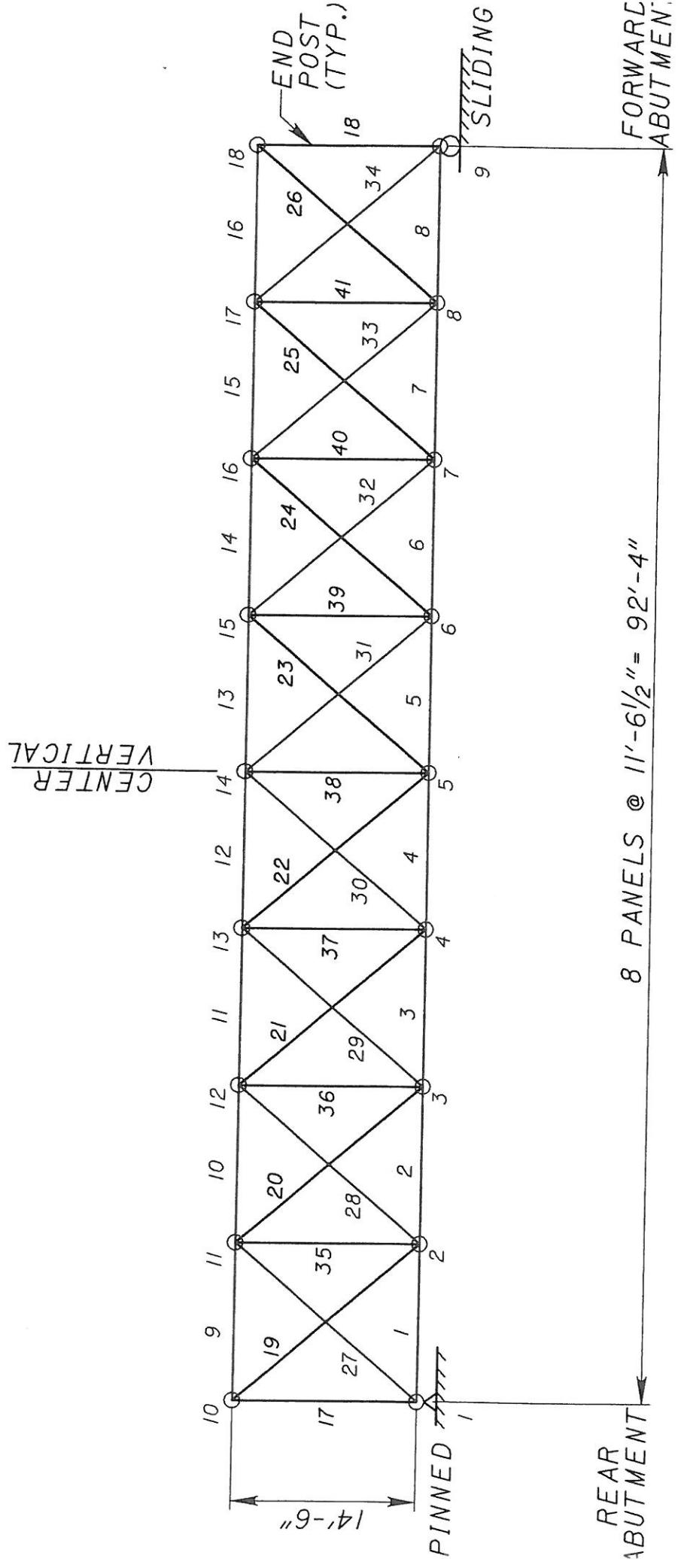
**Allowable Gross Vehicle Load (Tons)**

Loading Type	Vehicle Gross Load (tons)	Bending Stress	
		Inventory Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight	Operating Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight
H15-44	15	13.19	22.04
School Bus	13	18.02	30.09
Ohio 2F1	15	13.37	22.33
Ohio 3F1	23	14.41	24.07
Ohio 4F1	27	15.19	25.36
Ohio 5C1	40	25.90	43.25

Loading Type	Vehicle Gross Load (tons)	Shear Stress	
		Inventory Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight	Operating Allowable Gross Load (tons) =Rating Factor * Gross Vehicle Weight
H15-44	15	70.59	117.89
School Bus	13	96.39	160.97
Ohio 2F1	15	71.52	119.44
Ohio 3F1	23	77.09	128.74
Ohio 4F1	27	81.23	135.65
Ohio 5C1	40	138.54	231.36

— COMPRESSION DIAGONAL  
 — COUNTER  
 — VERTICAL ROD

○ JOINT NUMBER  
 — UPPER CHORD  
 — LOWER CHORD



8 PANELS @ 11'-6 1/2" = 92'-4"

PINNED

REAR ABUTMENT

CENTRE VERICAL

FORWARD ABUTMENT

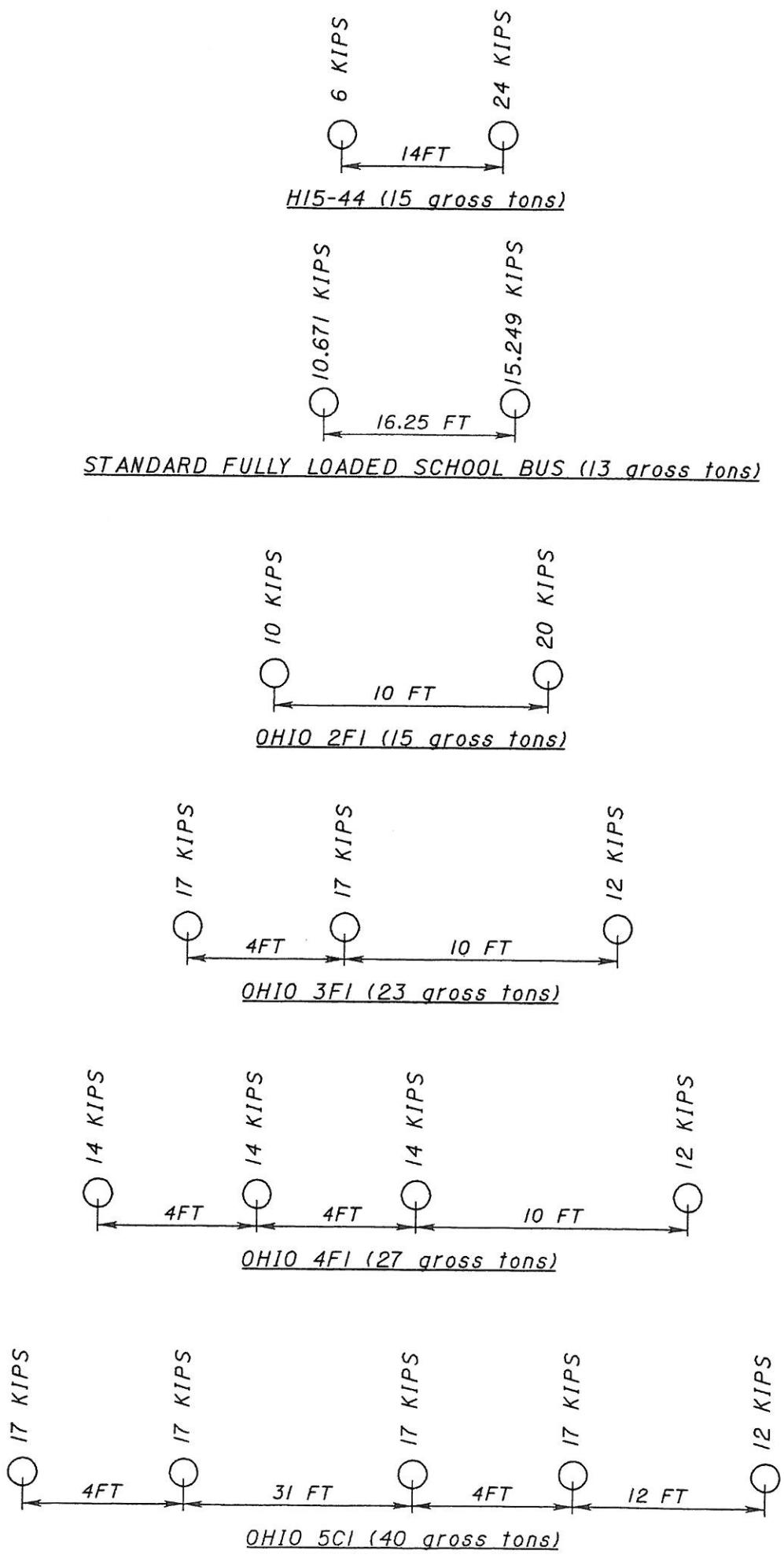
SLIDING

BRIDGE 38-0.20

FIGURE 1 (TRUSS MODEL)  
BICKHAM COVERED BRIDGE OVER

THE SOUTHERN TUE MOUNTAIN RIVER

BURGESS & NIPLE



3 RIDGE 38-0.20

FIGURE 2 (TRUCK TYPES)  
BICKHAM COVERED BRIDGE OVER

TRUE CENTER AND TIE RAIL SPACING

BURGESS & NIPPLE

**Allowable Member Stresses (psi)**  
**Eastern White Pine Sawn Lumber (1.)**

Sep-01

- White Pine for truss members is Select Structural  
(For  $d > 12"$ )  $CF = (12/d)^{1/9} = 1.0$  (not applicable to Bickham, because  $d <$
  - Applies to glued laminated members, not sawn lumber
  - Not applicable to timbers
  - For circular or diamond sections
  - Factors for CP (dead load) = Bickham U.C. 0.96  
Bickham Diag. 0.80
  - Based on a permanent D.L. and a ten year cumulative L.L. duration
  - Factors for CP (live load) = Bickham U.C. 0.96  
Bickham Diag. 0.77
  - Members are not incised
  - Allowable stress for wrought iron = 20,000 psi (per AASHTO)

Table 1

## BICKHAM COVERED BRIDGE TRUSS LOAD RATING ANALYSIS (H15 TRUCK)

LOGAN COUNTY, OHIO

## MEMBER PROPERTIES, FORCES, STRESSES AND RATING

By: M. Killian / T. Butz (Burgess & Niple)  
September-01

FILE: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSS.XLS

STAAD FILES: PB30099\ETC\ANALYSIS SUMMARY\STAADITBLU

WAAD FILES: PRE-00995/ETC ANALYSIS SUMMARY STAAD/STRUSSHS and TRUSSDELT

**CONTROLLING RATING:**

## ICKHAM COVERED BRIDGE TRUSS LOAD RATING ANALYSIS (BUS TRUCK)

GAN COUNTY, OHIO

MEMBER PROPERTIES, FORCES, STRESSES AND RATING

By: M. Killian / T. Butz (Burgess & Niple)  
September-01

FILE: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSS.XLS

\*\*AAD FILES: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSSBUS and trussd2

Member Description	Member No.	DIMENSIONS (inches)								PROPERTIES						A		B		C		D		E		F=D-E		G=C/A		H=[F/G]*Gross Tonnage		RATING (Bus) (TONS)			NDS REQUIREMENTS		COMMENTS		FINAL RATING (GROSS VEHICLE TONS)							
		outside member		outside rod	middle member	inside rod	inside member		full member		Joint deduct width (in.) (if any)?	Joint area (in**2)	DEAD LOAD		FORCES (Lbs. & Inches)		ALLOWABLE STRESS (PSI)		DEAD LOAD STRESS (PSI)		REMAINING STRENGTH (PSI)		LIVE LOAD STRESSES (PSI)		Member No.		Member Description		Gross Tonnage: 13		MZ & FX															
		width (w)	height (h)	diameter (d)	width (w)	height (h)	diameter (d)	width (w)	height (h)	area (in**2)	I (in**4)	weight (lb/inch)	FX	C/T	FY	MZ	MAX FX	C/T	MAX FY	MAX MZ	Ft' / Fc'	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	AXIAL	L. SHEAR	BENDING	Member No.	Member Description	AXIAL	L. SHEAR	BENDING	3.9.1 (F1) or 3.9.2 (Fc) (<1)	Interaction Rating (tons)									
Lower Chord	1	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	10757	T	398	55080	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	75.9	T	4.2	222.0	1	Lower Chord	102.3	T	195.5	61.0	0.46	—	61.0	
	2	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14584	T	191	3999	18444	T	782	60752	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	130.1	T	8.3	244.9	2		52.4	T	99.0	54.9	0.65	—	52.4	
	3	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	23045	T	535	59400	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	162.6	T	5.7	239.5	3		38.5	T	145.0	56.1	0.73	—	38.5	
	4	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	25553	T	300	31063	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	180.3	T	3.2	125.2	4		33.7	T	257.6	106.1	0.74	—	33.7	
	5	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	25553	T	300	31063	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	180.3	T	3.2	125.2	5		33.7	T	106.1	0.74	—	33.7		
	6	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	23045	T	535	59400	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	162.6	T	5.7	239.5	6		38.5	T	145.0	56.1	0.73	—	38.5	
	7	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	18444	T	782	60752	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	130.1	T	8.3	244.9	7		52.4	T	99.0	54.9	0.65	—	52.4	
	8	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	10757	T	398	55080	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	75.9	T	4.2	222.0	8		102.3	T	195.5	61.0	0.46	—	61.0	
Upper Chord	9	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	0	C	166	4580	0	C	274	37953	590	65	1,050	0	C	1.9	22.6	589.7	63.1	1,027.4	0.0	C	3.2	186.9	9	Upper Chord	255.7	T	71.5	0.20	—	—	Does not carry load	71.5
	10	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	14582	C	178	4580	10757	C	530	40502	590	65	1,050	113.7	C	2.1	22.6	476.0	62.9	1,027.4	83.9	C	6.2	199.5	10		73.8	C	132.0	67.0	0.54	—	67.0	
	11	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	24844	C	139	16879	353	40162	590	65	1,050	193.7	C	1.6	8.3	396.0	63.4	1,041.7	131.6	C	4.1	197.8	11	39.1	C	199.5	68.5	0.70	—	39.1				
	12	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	31051	C	157	4238	20047	C	167	17946	590	65	1,050	242.1	C	1.8	20.9	347.6	63.2	1,029.1	156.3	C	2.0	88.4	12	28.9	C	420.1	151.4	0.78	—	28.9		
	13	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	31051	C	157	4238	20047	C	167	17946	590	65	1,050	242.1	C	1.8	20.9	347.6	63.2	1,029.1	156.3	C	2.0	88.4	13	28.9	C	420.1	151.4	0.78</td				

## ICKHAM COVERED BRIDGE TRUSS LOAD RATING ANALYSIS (2F1 TRUCK)

MANUFACTURED IN OHIO

MEMBER PROPERTIES, FORCES, STRESSES AND RATING

FILE: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSS.XLS

September-01

\*\*AD FILES: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSS2F1 and trussdl3

Member No.	Dimensions (inches)										Properties										Forces (Lbs. & Inches)										Allowable Stress (PSI)										Dead Load Stress (PSI)										Remaining Strength (PSI)										Live Load Stresses (PSI)										H=[F/G]* Gross Tonnage									
	outside member	middle member	inside rod	inside member	full member	Joint deduct width (in.) (if any)?	Joint area (in.^2)	DEAD LOAD	2F1 LIVE LOAD	MAX FX	MAX CT	MAX FY	MAX MZ	FX	C/T	FY	MZ	FX	CT	FY	MZ	FX	CT	FY	MZ	FX	CT	VL	MAX.	FX	CT	VL	MAX.	FX	CT	VL	MAX.	FX	CT	VL	MAX.	Member No.	Member Description	Gross Tonnage: 15	MZ & FX	3.9.1 (F1) or 3.9.2 (Fc) <1	Interaction Rating (tons)																																	
	width (w)	height (h)	diameter (d)	width (w)	height (h)	diameter (d)	width (w)	height (h)	area (in.^2)	I (in.^4)	weight (lb/inch)	(If any)?	Joint area (in.^2)	FX	C/T	FY	MZ	FX	CT	FY	MZ	FX	CT	FY	MZ	FX	CT	VL	MAX.	FX	CT	VL	MAX.	FX	CT	VL	MAX.	FX	CT	VL	MAX.	Member No.	Member Description																																					
	(w)	(h)	(d)	(w)	(h)	(d)	(w)	(h)	(in.^2)	(in.^4)	(lb/inch)		(in.^2)	FX	C/T	FY	MZ	FX	CT	FY	MZ	FX	CT	FY	MZ	FX	CT	VL	MAX.	FX	CT	VL	MAX.	FX	CT	VL	MAX.	FX	CT	VL	MAX.	Member No.	Member Description																																					
Lower Chord	1	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	14182	T	622	86118	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	100.0	T	6.6	347.2	1	Lower Chord	89.5	T	144.3	45.0	0.61	—	45.0																																			
	2	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	22709	T	1215	92431	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	160.2	T	12.9	372.6	2	Lower Chord	49.1	T	73.5	41.6	0.80	—	41.6																																			
	3	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	28412	T	739	81318	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	200.4	T	7.8	327.8	3	Lower Chord	36.0	T	121.2	47.3	0.82	—	36.0																																			
	4	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	31317	T	417	43025	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	220.9	T	4.4	173.4	4	Lower Chord	31.7	T	213.7	88.4	0.84	—	31.7																																			
	5	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	31317	T	417	43025	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	220.9	T	4.4	173.4	5	Lower Chord	31.7	T	213.7	88.4	0.84	—	31.7																																			
	6	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	28412	T	739	81318	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	200.4	T	7.8	327.8	6	Lower Chord	36.0	T	121.2	47.3	0.82	—	36.0																																			
	7	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	22709	T	1215	92431	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	160.2	T	12.9	372.6	7	Lower Chord	49.1	T	73.5	41.6	0.80	—	41.6																																			
	8	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	14182	T	622	86118	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	100.0	T	6.6	347.2	8	Lower Chord	89.5	T	144.3	45.0	0.61	—	45.0																																			
Upper Chord	9	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	0	C	166	4580	0	C	427	59156	590	65	1,050	0.0	C	1.9	22.6	589.7	63.1	1,027.4	0.0	C	5.0	291.3	9	Upper Chord	189.3	C	189.3	52.9	0.30	—	52.9																																			
	10	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	14582	T	178	4580	14182	T	834	62357	590	65	1,050	113.7	C	2.1	22.6	476.0	62.9	1,027.4	110.6	C	9.8	307.1	10	Upper Chord	64.6	C	96.8	50.2	0.69	—	50.2																																			
	11	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	24844	C	139	1681	20560	C	499	55736	590	65	1,050	193.7	C	1.6	8.3	396.0	63.4	1,041.7	160.3	C	5.8	274.5	11	Upper Chord	37.0	C	162.8	56.9	0.79	—	37.0																																			
	12	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	12																																																																		

## BICKHAM COVERED BRIDGE TRUSS LOAD RATING ANALYSIS (3F1 TRUCK)

LOGAN COUNTY, OHIO

MEMBER PROPERTIES, FORCES, STRESSES AND RATING

By: M. Killian / T. Butz (Burgess & Niple)  
September-01

FILE: PR30099ETCANALYSIS SUMMARY\STAAD\TRUSS.XLS

STAAD FILES: PR30099ETCANALYSIS SUMMARY\STAAD\TRUSS3F1 and trussd4

Member Description	Member No.	DIMENSIONS (inches)								PROPERTIES						FORCES (Lbs. & Inches)				ALLOWABLE STRESS (PSI)				DEAD LOAD STRESS (PSI)				REMAINING STRENGTH (PSI)				LIVE LOAD STRESSES (PSI)				Member No.	H=[F/G]*Gross Tonnage				RATING (3F1) (TONS)		NDS REQUIREMENTS		COMMENTS		FINAL RATING (GROSS VEHICLE TONS)
		outside member width (w)	height (h)	outside rod diameter (d)	middle member width (w)	height (h)	inside rod diameter (d)	inside member width (w)	height (h)	full member			Joint deduct width (in.) (If any?)	Joint area (in.^2)	FX	C/T	FY	MZ	MAX FX	C/T	MAX FY	MAX MZ	Ft' / Fc'	Fy'	Fb'	AXIAL FX	L. SHEAR C/T	BENDING VL	MAX.	AXIAL FX	L. SHEAR C/T	BENDING VL	MAX.	AXIAL FX	L. SHEAR C/T	BENDING VL	MAX.	Gross Tonnage:	23	MZ & FX	3.9.1 (F) or 3.9.2 (Fc) <1	Interaction Rating (tons)					
Lower Chord	1	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	19826	T	899	124512	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	139.9	T	9.5	501.9	1	Lower Chord	98.2	T	153.0	47.7	0.82	—	47.7		
	2	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	34474	T	1750	132527	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	243.2	T	18.5	534.2	2	Lower Chord	49.6	T	78.2	44.5	1.02	22.3	Interaction greater than 1.0		
	3	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	43139	T	1067	117678	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	304.3	T	11.3	474.4	3	Lower Chord	36.3	T	128.6	50.1	1.04	21.9	Interaction greater than 1.0		
	4	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	47372	T	618	63701	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	334.2	T	6.5	256.8	4	Lower Chord	32.1	T	221.4	91.5	1.08	20.7	Interaction greater than 1.0		
	5	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	43139	T	1067	117678	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	304.3	T	11.3	474.4	5	Lower Chord	36.3	T	128.6	50.1	1.04	21.9	Interaction greater than 1.0		
	6	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	43139	T	1067	117678	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	243.2	T	18.5	534.2	6	Lower Chord	36.3	T	78.2	44.5	1.02	22.3	Interaction greater than 1.0		
	7	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	34474	T	1750	132527	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	139.9	T	9.5	501.9	7	Lower Chord	49.6	T	78.2	44.5	1.02	22.3	Interaction greater than 1.0		
	8	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	19826	T	899	124512	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	139.9	T	9.5	501.9	8	Lower Chord	98.2	T	153.0	47.7	0.82	—	47.7		
Upper Chord	9	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	0	C	166	4580	590	65	1,050	0.0	C	1.9	22.6	589.7	63.1	1,027.4	0.0	C	7.2	421.3	9	Upper Chord	200.7	C	56.1	0.42	—	—	Does not carry load						
	10	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	14582	C	1203	89785	590	65	1,050	113.7	C	2.1	22.6	476.0	62.9	1,027.4	154.6	C	14.1	442.2	10	Upper Chord	70.8	C	102.9	53.4	0.88	—	—						
	11	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	24844	C	139	1681	31212	C	725	80854	590	65	1,050	193.7	C	1.6	8.3	396.0	63.4	1,041.7	243.4	C	8.5	398.2	11	Upper Chord	37.4	C	172.0	60.2	0.98	—	—		
	12	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	31051	C	157	4238	4238	T	330	35826	590	65	1,050	242.1	C	1.8	20.9	347.6	63.2	1,029.1	290.2	C	3.9	176.4	12	Upper Chord	27.5	C	134.2	10.9	19.8	—	Interaction greater than 1.0		
	13	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	31051	C	157	4238	4238	T	330	35826	590	65	1,050	242.1	C	1.8	20.9	347.6	63.2	1,029.1	290.2	C	3.9	176.4	13	Upper Chord	27.5	C	134.2	10.9	19.8	—	Interaction greater than 1.0		
	14	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.0																																		

## BICKHAM COVERED BRIDGE TRUSS LOAD RATING ANALYSIS (4F1 TRUCK)

LOGAN COUNTY, OHIO

MEMBER PROPERTIES, FORCES, STRESSES AND RATING

By: M. Kilian / T. Butz (Burgess & Niple)  
September-01  
FILE: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSS.XLS  
STAAD FILES: PR30099\ETC\ANALYSIS SUMMARY\STAAD\TRUSS4F1 and trussd15

Member No.	Description	DIMENSIONS (inches)										PROPERTIES						FORCES (Lbs. & Inches)				ALLOWABLE STRESS (PSI)				DEAD LOAD STRESS (PSI)				REMAINING STRENGTH (PSI)				LIVE LOAD STRESSES (PSI)				Member No.	H=[F/G]*Gross Tonnage										RATING (4F1) (TONS)				NDS REQUIREMENTS				COMMENTS				FINAL RATING (GROSS VEHICLE TONS)			
		width (w)	height (h)	width (w)	height (h)	width (w)	height (h)	width (w)	height (h)	width (w)	height (h)	area (in.^2)	I (in.^4)	weight (lb/inch)	FX	C/T	FY	MZ	MAX FX	C/T	MAX FY	MAX MZ	F <sub>t'</sub> /F <sub>c'</sub>	F <sub>y'</sub>	F <sub>b'</sub>	FX	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	Member Description	Gross Tonnage:	27	MZ & FX	3.9.1 (Fc) or 3.9.2 (Fc) <1	Interaction Rating (tons)	—	51.4						
		width (w)	height (h)	diameter (d)	width (w)	height (h)	diameter (d)	width (w)	height (h)	diameter (d)	width (w)	area (in.^2)	I (in.^4)	weight (lb/inch)	FX	C/T	FY	MZ	MAX FX	C/T	MAX FY	MAX MZ	F <sub>t'</sub> /F <sub>c'</sub>	F <sub>y'</sub>	F <sub>b'</sub>	FX	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	Member Description	H=[F/G]*Gross Tonnage	RATING (4F1) (TONS)	NDS REQUIREMENTS	COMMENTS	FINAL RATING (GROSS VEHICLE TONS)								
Lower Chord	1	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	22909	T	980	135760	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	161.6	T	10.4	547.3	1	Lower Chord	99.8	T	164.7	51.4	0.89	—	51.4																			
	2	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14584	T	191	3999	39759	T	1915	146101	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	280.5	T	20.3	589.0	2	Lower Chord	50.5	T	83.9	47.4	1.12	23.2	Interaction greater than 1.0																			
	3	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	49881	T	1203	132773	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	351.9	T	12.7	535.2	3	Lower Chord	36.9	T	134.0	52.2	1.15	21.9	Interaction greater than 1.0																			
	4	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	54847	T	695	71731	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	386.9	T	7.4	289.2	4	Lower Chord	32.6	T	231.1	95.4	1.19	20.8	Interaction greater than 1.0																			
	5	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	49881	T	1203	132773	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,033.9	351.9	T	12.7	535.2	5	Lower Chord	32.6	T	231.1	95.4	1.19	20.8	Interaction greater than 1.0																			
	6	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	191	3999	39759	T	1915	146101	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,033.9	280.5	T	20.3	589.0	6	Lower Chord	36.9	T	134.0	52.2	1.15	21.9	Interaction greater than 1.0																			
	7	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14584	T	162	2061	22909	T	980	135760	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	161.6	T	10.4	547.3	7	Lower Chord	50.5	T	83.9	47.4	1.12	23.2	Interaction greater than 1.0																			
	8	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	22909	T	980	135760	700	65	1,050	102.9	T	1.7	8.3	597.1	63.3	1,041.7	161.6	T	10.4	547.3	8	Lower Chord	99.8	T	164.7	51.4	0.89	—	51.4																			
Upper Chord	9	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	0	C	166	4580	0	C	673	93225	590	65	1,050	0.0	C	1.9	22.6	589.7	63.1	1,027.4	0.0	C	7.9	459.1	9	Upper Chord	NO LOAD	C	216.2	60.4	0.46	—	Does not carry load	60.4																		
	10	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	14582	C	178	4580	22909	C	1314	98341	590	65	1,050	113.7	C	2.1	22.6	476.0	62.9	1,027.4	178.6	C	15.4	484.3	10	Upper Chord	71.9	C	110.5	57.3	0.96	—	Interaction greater than 1.0	57.3																		
	11	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	24844	C	139	1681	36149	C	804	90430	590	65	1,050	193.7	C	1.6	8.3	396.0	63.4	1,041.7	281.9	C	9.4	445.3	11	Upper Chord	37.9	C	181.9	63.2	1.08	24.3	Interaction greater than 1.0																			
	12	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	31051	C	157	4238	40392</																																													

## BICKHAM COVERED BRIDGE TRUSS LOAD RATING ANALYSIS (SC1 TRUCK)

LOGAN COUNTY, OHIO

MEMBER PROPERTIES, FORCES, STRESSES AND RATING

By: M. Killian / T. Butz (Burgess & Niple)

September-01

FILE: PR300991ETCANALYSIS SUMMARY\STAAD\TRUSS.XLS

STAAD FILES: PR300991ETCANALYSIS SUMMARY\STAAD\TRUSS5C1 and trussd16

Member Description	Member No.	DIMENSIONS (inches)								PROPERTIES						A			B			C			D			E			F=D-E			G=C/A			H=[F/G]*Gross Tonnage			RATING (SC1) (TONS)			NDS REQUIREMENTS		COMMENTS		FINAL RATING (GROSS VEHICLE TONS)
		outside member		outside rod		middle member		inside rod		inside member		full member			Joint deduct width (in.) (if any)?		Joint area (in.^2)		DEAD LOAD			SCI LIVE LOAD			ALLOWABLE STRESS (PSI)			DEAD LOAD STRESS (PSI)			REMAINING STRENGTH (PSI)			LIVE LOAD STRESSES (PSI)			Gross Tonnage:			Rating (SC1) (TONS)			MZ & FX				
		width (w)	height (h)	diameter (d)	width (w)	height (h)	diameter (d)	width (w)	height (h)	area (in.^2)	I (in.^4)	weight (lb/inch)	MAX FX	C/T	FY	MZ	MAX C/T	MAX FY	MAX MZ	Ft'/Fc'	Fv'	Fb'	AXIAL	L. SHEAR	BENDING	AXIAL	L. SHEAR	BENDING	AXIAL	L. SHEAR	BENDING	FX	C/T	VL	MAX.	FX	VL	MAX.	FX	C/T	VL	MAX.	FX	C/T	VL	MAX.	3.9.1 (F1) or Interaction
Lower Chord	1	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	25818	T	874	121046	700	65	1,050	102.9	T	1.7	83	597.1	63.3	1,041.7	182.1	T	9.2	488.0	1	Lower Chord	131.1	T	273.7	85.4	0.88	—	85.4		
	2	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	4417	T	1681	127145	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,035.9	313.4	T	17.8	512.6	2		67.0	T	141.6	80.7	1.13	34.4	34.4		
	3	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	55585	T	1129	122928	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,035.9	392.1	T	11.9	495.6	3		49.1	T	211.5	83.5	1.29	27.6	27.6		
	4	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	33038	T	195	6987	58883	T	776	81676	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	415.4	T	8.2	329.3	4		45.0	T	306.4	124.1	1.22	29.6	29.6		
	5	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	55585	T	1129	122928	700	65	1,050	233.1	T	2.1	28.2	466.9	62.9	1,021.8	415.4	T	8.2	329.3	4		45.0	T	306.4	124.1	1.22	29.6	29.6		
	6	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	31051	T	173	3999	55585	T	1129	122928	700	65	1,050	219.1	T	1.8	16.1	480.9	63.2	1,035.9	392.1	T	11.9	495.6	6		49.1	T	211.5	83.5	1.29	27.6	27.6		
	7	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	24844	T	191	3999	4417	T	1681	127145	700	65	1,050	175.3	T	2.0	16.1	524.7	63.0	1,035.9	313.4	T	17.8	512.6	7		67.0	T	141.6	80.7	1.13	34.4	34.4		
	8	4.50	10.50	0.00	4.50	10.50	0.00	4.50	10.50	141.75	1,302.33	3.94	0.00	141.75	14582	T	162	2061	25818	T	874	121046	700	65	1,050	102.9	T	1.7	83	597.1	63.3	1,041.7	182.1	T	9.2	488.0	8		131.1	T	273.7	85.4	0.88	—	85.4		
Upper Chord	9	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	0	C	166	4580	0	C	606	83916	590	65	1,050	0.0	C	1.9	22.6	589.7	63.1	1,027.4	0.0	C	7.1	413.3	9	Upper Chord	NO LOAD	C	355.9	99.4	0.42	—	99.4		
	10	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	14582	C	178	4580	25818	C	1153	86015	590	65	1,050	113.7	C	2.1	22.6	476.0	62.9	1,027.4	201.3	C	13.5	423.6	10		94.6	C	186.5	97.0	0.95	—	94.6		
	11	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	24844	C	139	1681	40325	C	727	79176	590	65	1,050	193.7	C	1.6	83	396.0	63.4	1,041.7	314.4	C	8.5	389.9	11		38.4	C	298.1	106.9	1.15	32.4	32.4		
	12	4.50	9.50	0.00	4.50	9.50	0.00	4.50	9.50	128.25	964.55	3.56	0.00	128.25	31051	C	157	4238	46392	C	437	47964	590	65	1,050	242.1	C	1.8	20.9	347.6	63.2	1,029.1	361.7	C	5.1	236.2	12		38.4	C	494.3	174.3	1.21	29.6			